## Hoop and spring oscillator problem.

Originally appeared at: http://sites.google.com/site/peeterjoot/math2010/hoopSpring.pdf

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## 1. Motivation.

Nolan was attempting to setup and solve the equations for the following system (1)

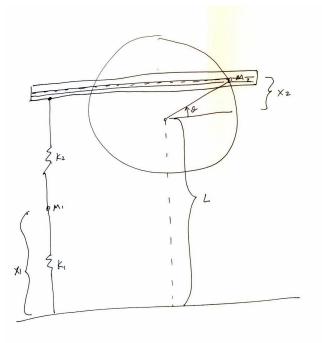


Figure 1: Coupled hoop and spring system.

One mass is connected between two springs to a bar. That bar moves up and down as forced by the motion of the other mass along a immovable hoop. While Nolan didn't include any gravitational force in his potential terms (ie: system lying on a table perhaps) it doesn't take much more to include that, and I'll do so. I also include the distance *L* to the center of the hoop, which I believe required.

## 2. Guts

The Lagrangian can be written by inspection. Writing  $x = x_1$ , and  $x_2 = R \sin \theta$ , we have

$$\mathcal{L} = \frac{1}{2}m_1\dot{x}^2 + \frac{1}{2}m_2R^2\dot{\theta}^2 - \frac{1}{2}k_1x^2 - \frac{1}{2}k_2(L + R\sin\theta - x)^2 - m_1gx - m_2g(L + R\sin\theta).$$
(1)

Evaluation of the Euler-Lagrange equations gives

$$m_1 \ddot{x} = -k_1 x + k_2 (L + R \sin \theta - x) - m_1 g$$
(2a)

$$m_2 R^2 \ddot{\theta} = -k_2 (L + R \sin \theta - x) R \cos \theta - m_2 g R \cos \theta, \qquad (2b)$$

or

$$\ddot{x} = -x\frac{k_1 + k_2}{m_1} + \frac{k_2 R \sin \theta}{m_1} - g + \frac{k_2 L}{m_1}$$
(3a)

$$\ddot{\theta} = -\frac{1}{R} \left( \frac{k_2}{m_2} \left( L + R \sin \theta - x \right) + g \right) \cos \theta.$$
(3b)

Just like any other coupled pendulum system, this one is non-linear. There's no obvious way to solve this in closed form, but we could determine a solution in the neighborhood of a point  $(x, \theta) = (x_0, \theta_0)$ . Let's switch our dynamical variables to ones that express the deviation from the initial point  $\delta x = x - x_0$ , and  $\delta \theta = \theta - \theta_0$ , with  $u = (\delta x)'$ , and  $v = (\delta \theta)'$ . Our system then takes the form

$$u' = f(x,\theta) = -x\frac{k_1 + k_2}{m_1} + \frac{k_2 R \sin \theta}{m_1} - g + \frac{k_2 L}{m_1}$$
(4a)

$$v' = g(x,\theta) = -\frac{1}{R} \left( \frac{k_2}{m_2} \left( L + R\sin\theta - x \right) + g \right) \cos\theta$$
(4b)

$$(\delta x)' = u \tag{4c}$$

$$(\delta\theta)' = v. \tag{4d}$$

We can use a first order Taylor approximation of the form  $f(x,\theta) = f(x_0,\theta_0) + f_x(x_0,\theta_0)(\delta x) + f_\theta(x_0,\theta_0)(\delta \theta)$ . So, to first order, our system has the approximation

$$u' = -x_0 \frac{k_1 + k_2}{m_1} + \frac{k_2 R \sin \theta_0}{m_1} - g + \frac{k_2 L}{m_1} - (\delta x) \frac{k_1 + k_2}{m_1} + \frac{k_2 R \cos \theta_0}{m_1} (\delta \theta)$$
(5a)  
$$v' = -\frac{1}{R} \left( \frac{k_2}{m_2} \left( L + R \sin \theta_0 - x_0 \right) + g \right) \cos \theta_0 + \frac{k_2 \cos \theta_0}{m_2 R} (\delta x) - \frac{1}{R} \left( \frac{k_2}{m_2} \left( (L - x_0) \sin \theta_0 + R \right) + g \sin \theta_0 \right) (\delta \theta)$$
(5b)

$$\begin{aligned} (\delta x)' &= u \\ (\delta \theta)' &= v. \end{aligned}$$
 (5c) (5d)

This would be tidier in matrix form with  $\mathbf{x} = (u, v, \delta x, \delta \theta)$ 

$$\mathbf{x}' = \begin{bmatrix} -x_0 \frac{k_1 + k_2}{m_1} + \frac{k_2 R \sin \theta_0}{m_1} - g + \frac{k_2 L}{m_1} \\ -\frac{1}{R} \left( \frac{k_2}{m_2} \left( L + R \sin \theta_0 - x_0 \right) + g \right) \cos \theta_0 \\ 0 \end{bmatrix} + \begin{bmatrix} 0 & 0 & -\frac{k_1 + k_2}{m_1} & \frac{k_2 R \cos \theta_0}{m_1} \\ 0 & 0 & \frac{k_2 \cos \theta_0}{m_2 R} & -\frac{1}{R} \left( \frac{k_2}{m_2} \left( \left( L - x_0 \right) \sin \theta_0 + R \right) + g \sin \theta_0 \right) \\ 1 & 0 & 0 \\ 0 & 1 & 0 & 0 \end{bmatrix} \mathbf{x}$$
(6)

This reduces the problem to the solutions of first order equations of the form

$$\mathbf{x}' = \mathbf{a} + \begin{bmatrix} 0 & A \\ I & 0 \end{bmatrix} \mathbf{x} = \mathbf{a} + \mathbf{B}\mathbf{x}$$
(7)

where **a**, and A are constant matrices. Such a matrix equation has the solution

$$\mathbf{x} = e^{Bt} \mathbf{x}_0 + (e^{Bt} - I)B^{-1} \mathbf{a},\tag{8}$$

but the zeros in *B* should allow the exponential and inverse to be calculated with less work. That inverse is readily verified to be

$$B^{-1} = \begin{bmatrix} 0 & I \\ A^{-1} & 0 \end{bmatrix}.$$
 (9)

It is also not hard to show that

$$B^{2n} = \begin{bmatrix} A^n & 0\\ 0 & A^n \end{bmatrix}$$
(10a)

$$B^{2n+1} = \begin{bmatrix} 0 & A^{n+1} \\ A^n & 0 \end{bmatrix}.$$
 (10b)

Together this allows for the power series expansion

$$e^{Bt} = \begin{bmatrix} \cosh(t\sqrt{A}) & \sinh(t\sqrt{A}) \\ \sinh(t\sqrt{A})\frac{1}{\sqrt{A}} & \cosh(t\sqrt{A}) \end{bmatrix}.$$
 (11)

All of the remaining sub matrix expansions should be straightforward to calculate provided the eigenvalues and vectors of *A* are calculated. Specifically, suppose that we have

$$A = U \begin{bmatrix} \lambda_1 & 0\\ 0 & \lambda_2 \end{bmatrix} U^{-1}.$$
 (12)

Then all the perhaps non-obvious functions of matrixes expand to just

$$A^{-1} = U \begin{bmatrix} \lambda_1^{-1} & 0\\ 0 & \lambda_2^{-1} \end{bmatrix} U^{-1}$$
(13a)

$$\sqrt{A} = U \begin{bmatrix} \sqrt{\lambda_1} & 0\\ 0 & \sqrt{\lambda_2} \end{bmatrix} U^{-1}$$
(13b)

$$\cosh(t\sqrt{A}) = U \begin{bmatrix} \cosh(t\sqrt{\lambda_1}) & 0\\ 0 & \cosh(t\sqrt{\lambda_2}) \end{bmatrix} U^{-1}$$
(13c)

$$\sinh(t\sqrt{A}) = U \begin{bmatrix} \sinh(t\sqrt{\lambda_1}) & 0\\ 0 & \sinh(t\sqrt{\lambda_2}) \end{bmatrix} U^{-1}$$
(13d)

$$\sinh(t\sqrt{A})\frac{1}{\sqrt{A}} = U \begin{bmatrix} \sinh(t\sqrt{\lambda_1})/\sqrt{\lambda_1} & 0\\ 0 & \sinh(t\sqrt{\lambda_2})/\sqrt{\lambda_2} \end{bmatrix} U^{-1}.$$
 (13e)

An interesting question would be how are the eigenvalues and eigenvectors changed with each small change to the initial position  $\mathbf{x}_0$  in phase space. Can these be related to each other?